

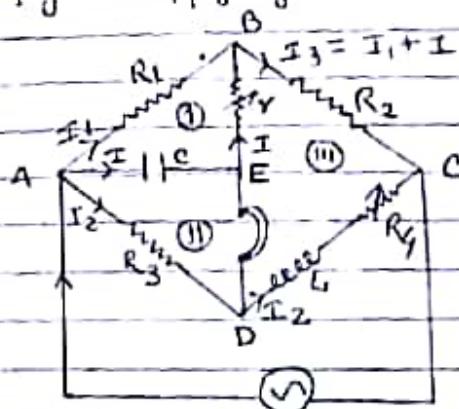
Anderson Bridge

A-2(II) Paper IV

This is the modified form of Maxwell's L/C bridge.

The double balance is obtained by after adjusting resistances only, the standard condenser being invariably.

Anderson's bridge shown in fig is formed by placing the condenser C and a non inductive resistance r in series with the condenser, the combination being parallel with R_1 ; the other components and detector are placed as shown in fig. At the time of balance E and D are at the same potential and let the current-vectors in the different parts of the bridge be as indicated in fig. Applying Kirchhoff's law we have



$$R_1 I_1 - \left(r + \frac{1}{j\omega C}\right) I = 0 \quad [\text{for Loop I}] \quad (1)$$

$$\frac{1}{j\omega C} \cdot I - R_3 I_2 = 0 \quad [\text{for Loop II}] \quad (2)$$

$$R_2 (I_1 + I) + r I - (j\omega L + R_4) I_2 = 0 \quad [\text{for Loop III}] \quad (3)$$

Substituting the value of I_1 & I_2 from equn (1) & (2) in equn (3) we have,

$$\frac{R_2}{R_1} \left(r + \frac{1}{j\omega C}\right) I + R_2 I - \frac{(j\omega L + R_4) I_2}{j\omega C R_3} + r I = 0 \quad (4)$$

Equating real & imaginary parts, we have

$$\frac{R_2}{R_1} r + R_2 - \frac{L}{CR_3} + r = 0$$

$$\text{or } L = CR_3 \left[\frac{R_2}{R_1} r + R_2 + r \right]$$

$$= CR_3 \left[r \left(1 + \frac{R_2}{R_1} \right) + R_2 \right] \quad (5)$$

$$\text{and } \frac{R_2}{R_{1\text{wc}}} - \frac{R_4}{R_{3\text{wc}}} = 0 \text{ or } \frac{R_1}{R_2} = \frac{R_3}{R_4} \quad \text{--- (6)} \quad 2$$

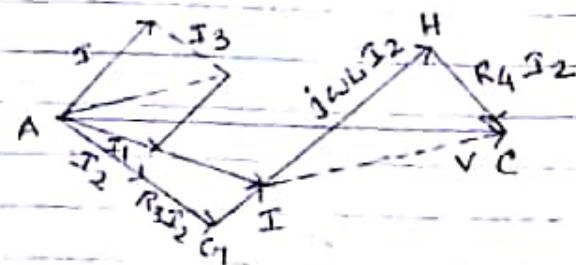
These conditions are independent of the frequency of the source and can be satisfied independently of each other by adjusting R_4 in the latter case and τ in the former case. Eqn (5) shows that balance is possible only when $L > C R_2 R_3$ otherwise τ will be negligible negative. Since there is no other inductance all mutual reactions between neighbouring inductance is avoided.

It is best to use $R_1 : R_2 = 1:1$

The formula then reduces to

$$R_3 = R_4 \text{ and } L = CR_3(2\tau + R_2) \quad \text{--- (7)}$$

The vector diagram for the Anderson bridge is shown below. If in it AC is \vec{V} , the potential vector for the applied voltage. If I_2 represents the current in A-DC, then $AC_1 = R_3 I_2$ and $C_1 H = j\omega L I_2$ and $HC = R_4 I_2$, so that $HC \perp AC_1$ and



$CH \perp AC_1$ or $HC \perp AC_1$. Since the potential of E is the same as that of D, hence

$$VE = VAD$$

$$\text{or } (\pm j\omega C)I = R_3 I_2$$

This relation shows that I is in quadrature with I_2 . If we draw $C_1 I = RI$ then the vector AI is $R_1 I_1$.

The vector IC is $R_2 I_3 = R_2(I_1 + I)$.

First of all the circuit is arranged as simple Wheatstone Bridge connecting the inductance in the 4th arm CD. The resistance R_1 and R_2 are fixed to 10 ohm each and R_3 is varied until the galvanometer deflection changes direction. The expected value is calculated with the formula (6). The expt. is

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repeated with $\frac{R_1}{R_2} = 10$ and 100 and the actual resistance in the inductance arm R_2 is calculated.

Now R_1 and R_2 are readjusted to the ratio 10 : 10 and a fractional resistance R' is placed in series with the inductance. Now R_3 and R_4 , R' are varied for no deflection in the galvanometer. In this case

$$R_1 + R' = R_4 = R_3. \quad \text{To increase the sensitivity}$$

the resistances are so arranged that $R_1 = R_2 = \frac{1}{2} R_3$

Now galvanometer and D.C source are replaced by Headphone and A.C source respectively and capacitance C and resistance r are inserted as shown in fig. R_1, R_2, R_3 and R_4 are kept as such and the bridge is balanced for minimum sound with the help of resistance r . The expt. may be repeated by taking different capacitances. Substituting these values in eqn (7) self-inductance of a given coil can be calculated.